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**IN-LINE
OXYGEN SENSORS
FOR THE GLASS INDUSTRY**
in glass melt, atmosphere and tin bath

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In-line Oxygen Sensors for the Glass Industry, in Glass Melt, Atmosphere and Tin Bath

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Activity & products


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Read-Ox & Consultancy BV established in 2001
In-line electrochemical sensors for glass melts, metal melts and molten salts




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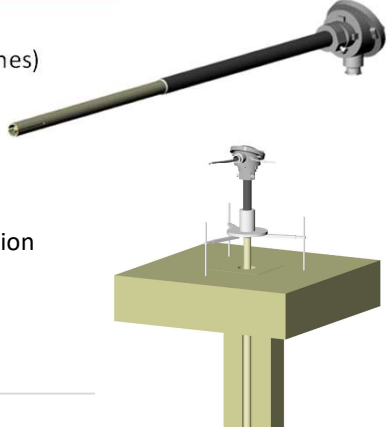
Product overview

for the glass industry




• **Glass melt** redox sensor
(for the glass melt in the feeder channel, forehearth or canal)

- **Tin bath** oxygen sensors (in float glass production lines)
 - Tin melt oxygen sensor
 - Atmosphere oxygen sensor
 - Tin melt hydrogen sensor
- **Atmosphere** oxygen sensor for monitoring combustion process ($T_{\max} = 1650^{\circ}\text{C}$)
 - Crown
 - Flue gas channel / Regenerator



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Contents

- Importance of redox affecting glass melt /product properties
- In-line redox measuring system
 - Measuring principle
- Redox control (examples)
 - Heat transfer
 - Glass colour (container glass)
 - Emerald green*
 - Olive/Dead leaf*
 - Antique green*
- Iron-ratio (cold glass) as sensor output
- Concluding remarks / New developments

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Oxidation state of glass melt

Introduction

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Oxidation state of the melt determines the valency state of the Multi-valent Ions (MI) :

$$MI^{x+} + n/4 O_2 \leftrightarrow MI^{(x+n)+} + n/2 O^{2-}$$

	Reduced melt Low valency	Oxidised melt High valency
Iron	Fe ²⁺ FeO	Fe ³⁺ Fe ₂ O ₃
Sulfur	S ²⁻ Na ₂ S	S ⁴⁺ SO ₂ S ⁶⁺ Na ₂ SO ₄
Chromium	Cr ²⁺ CrO	Cr ³⁺ Cr ₂ O ₃ Cr ⁶⁺ CrO ₃

➔ Redox ➔ valency state multivalent ion ➔ glass properties

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Effect of the redox state on properties

Overview

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- **Gas production of the melt**
 - Fining behaviour $SO_4^{2-} + 2 Fe^{2+} \rightarrow SO_2(g) + 2 Fe^{3+} + 2 O^{2-}$
 - Foaming behaviour $SO_4^{2-} \rightarrow SO_2(g) + 1/2 O_2(g) + O^{2-}$
- **Heat transfer** *Fe²⁺: broad absorption band in near infrared*
 - Energy consumption
 - Temperature distribution / glass melt flow patterns in melting tank
 - Bottom temperatures (seed count and release of precipitates)
 - Crown temperatures (furnace lifetime)
- **Forming process via cooling rate**
 - Gob & (pre)form cooling rate in mould (e.g. surface cracks)
 - Fiber glass: cooling rate of fibers (Fiber breaks / hr)
- **Glass colour/optical properties**
 - Multivalent ions in solution Fe²⁺ Fe³⁺ Fe²⁺/Fe³⁺ Cr²⁺ Cr³⁺ Cr⁶⁺ Fe³⁺-S²⁻
 - UV absorption (Fe³⁺, Cr⁶⁺, Ce⁴⁺)

➔ Every glass melt type has its optimal redox state

➔ Redox variations destabilise the glass melting process

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$SO_4^{2-} \xrightarrow{T} SO_2 + \frac{1}{2}O_2 + O^{2-}$
 $2Fe^{2+} \xrightarrow{\quad} 2Fe^{3+} + O^{2-}$

Redox state & Fining

Fining by the sulfate–iron fining reaction:
 SO_4^{2-} is reduced by Fe^{2+} (1100-1400°C) producing SO_2 fining gas inflating remaining CO_2 seeds

Redox controls:

- T_{onset} fining
- Amount of fining gas produced

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$SO_4^{2-} \xrightarrow{T} SO_2 + \frac{1}{2}O_2 + O^{2-}$

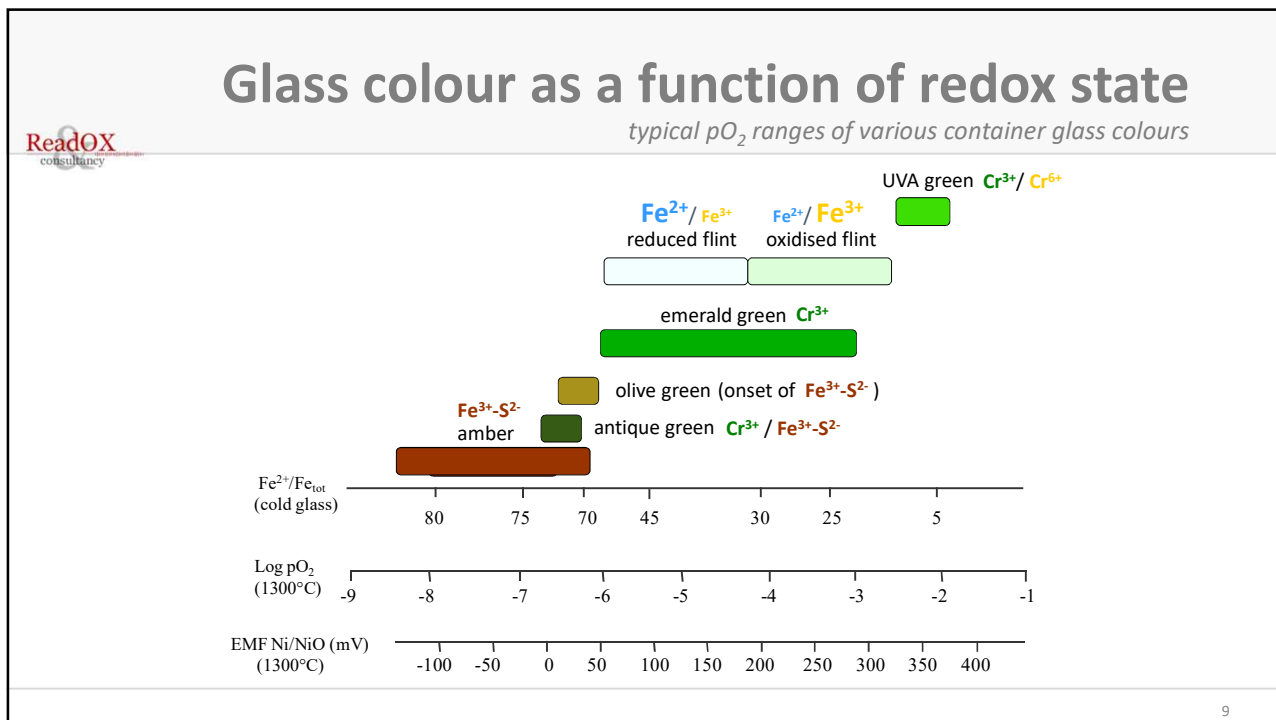
Redox state & Foaming

Foaming by thermal sulfate decomposition:
in oxidised glass melts ($T > 1400$ °C) producing large amounts of SO_2 and O_2 causing vigorous foaming

Redox controls:

- T_{onset} foaming
- Amount of foaming gas produced

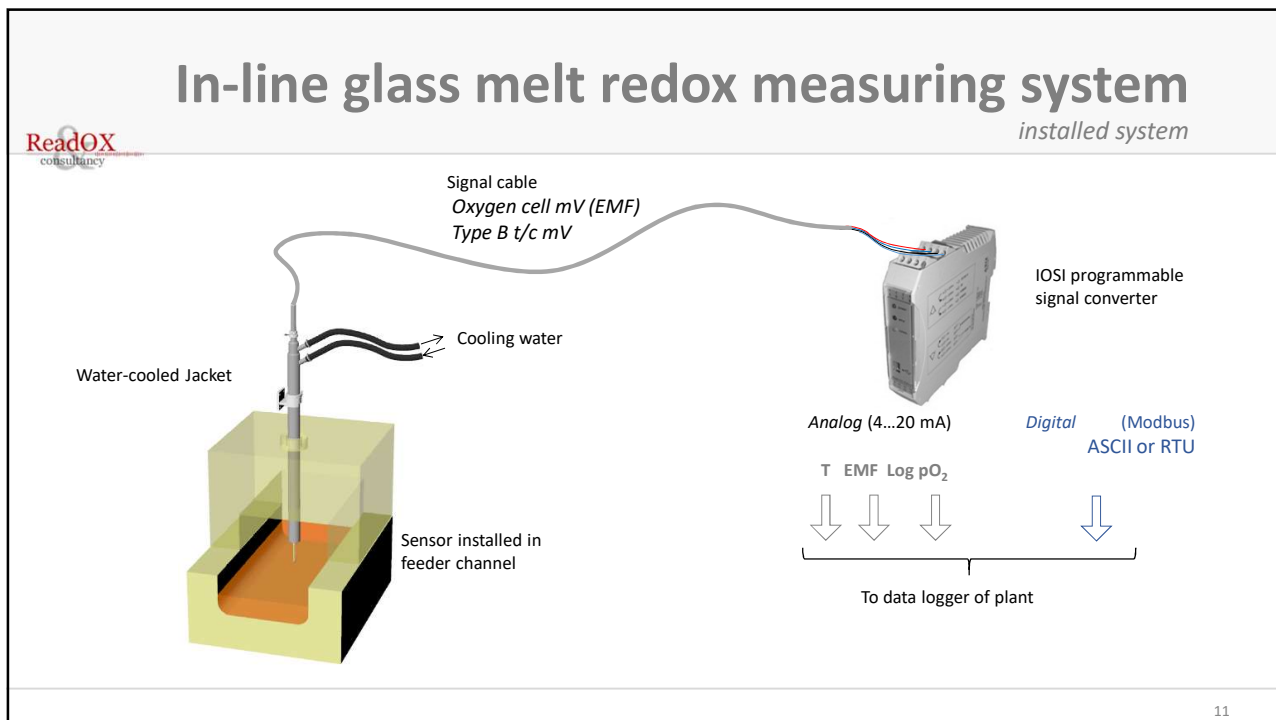
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In-line glass melt redox measuring system

programmable IOSI converter and PC software

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Custom calculations: Glass Melt Redox (Custom calculation example)

Inputs	Outputs	Constants	Registers
1	Name	Value	
2	T-offset	0	
3	T-span	2500	
4	t/c	4	
5	20mA	20	
6	mV-span	16	
7	log pO ₂ A	-20.171	
8	log pO ₂ B	-30620	
9	log pO ₂ C	9.33	
10	log pO ₂ -offset	-12	
11	log pO ₂ -span	12	
12			
13	mV-span	1000	
14	mV-offset	0	
15			
16	K	273.15	

Configuration:

- calculations
- analog output ranges

Actual values

Calculation: linear Vcc voltage: 4.9 [V]
 Firmware: 0.50 USB bus voltage: 5.1 [V]
 Serial no: 5320752 Calculation time: 1 [ms]

Raw values:
 Ox cell: 452.46 [mV]
 TC: 37.898 [mV]
 Cold J: 28.1 [C]
 I-in: 5.68 [mA]

Recording

Log configuration: datalogging
 Results file: Log190812104629.csv
 New results file after: 1 hour
 Log interval: 1 second (1 days max)
 Averaging: 5 minutes

Graph: Minimum Maximum
 Ox cell: 0 1000 [mV]
 TC: 0 25 [mV]
 CJC: 0 40 [C]
 In: 0 20 [mA]

Screen time base: 5 minutes

Start Stop

USB port

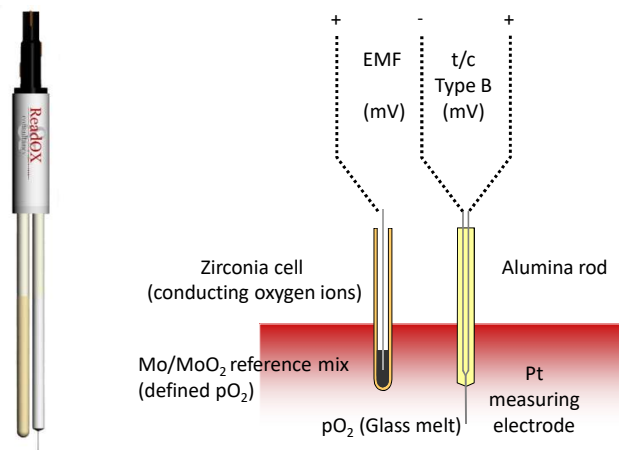
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Redox sensor: measuring principle



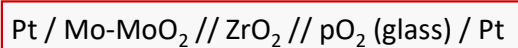
Oxygen sensor is an electrochemical cell: output Electro Motive Force (EMF)



Redox sensor: measuring principle



Electrochemical cell



- Mo-MoO₂ reference material
- ZrO₂ solid electrolyte
- pO₂ oxygen activity in the glass melt
- Pt measuring electrode

Nernst equation:

$$\text{EMF} = \frac{RT}{nF} \cdot \ln \frac{\text{pO}_2(\text{glass})}{\text{pO}_2(\text{ref. Mo/MoO}_2)}$$

$$\log \text{pO}_2(\text{Mo/MoO}_2) = -\frac{30620}{(T+273)} + 9.33$$

$$\log \text{pO}_2(\text{glass}) = \frac{20.171 \cdot \text{EMF} - 30620}{T + 273} + 9.33$$

EMF (mV)
T (°C)
pO₂ (bar)

Preprogrammed
in the IOSI signal converter



In-line glass melt redox measuring system

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- Simple design, low-cost
- Flexible in location
- Exchangeable redox sensor (lifetime of about 6 weeks at 1150-1200°C)
- Easy sensor exchange (takes 10 to 15 minutes)
- No reference gas flushing due to solid reference (No gas bottles near furnace)
- Repair and part exchange can be done by personnel of the production facility



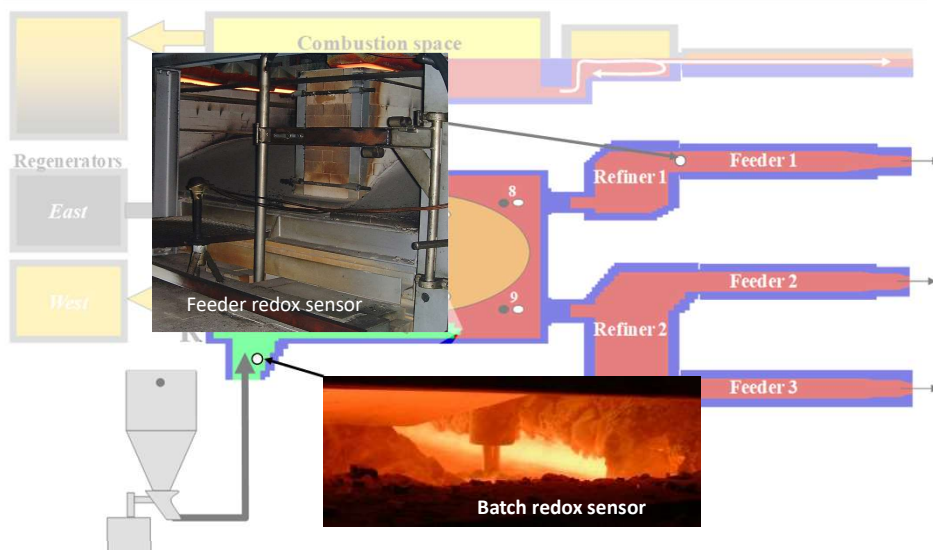
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Redox measurements in industrial furnace

container glass

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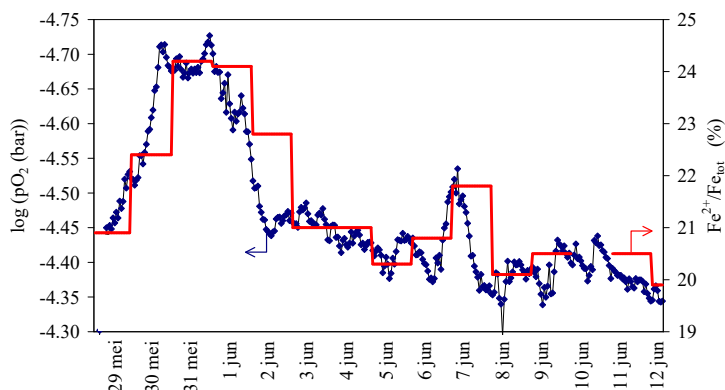
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Redox measurements in industrial furnace



advantage of a continuous redox measurement

log pO₂ (feeder sensor) versus daily analysed Fe²⁺/Fe_{tot} ratio:



Advantages in-line redox sensor:

- Time gain for control (max. ≈ 24 hr!)
- Redox state continuously available Level, direction and rate of change (also when laboratory is closed!)

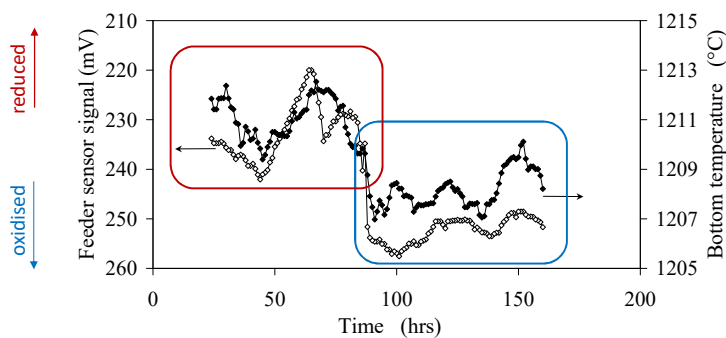
- ➔ Operator is more confident and uses signal for batch redox number corrections
- ➔ Foreign cullet share could be increased by 5% (saving batch costs and energy costs!)

Redox control – Heat transfer



Relation heat transfer - redox / Emerald green container glass

Use of in-line redox sensor revealed following relation*:



- Oxidised melt → low bottom temperatures (bad heat transfer)
- Reduced melt → high bottom temperatures (good heat transfer)

* in this particular emerald green container glass furnace (air fuel fired)

Redox control – Heat transfer

Relation heat transfer - redox : better process control

Corrective measures to restore bottom temperature:

- Case 1** – increase overhead firing
- Case 2** – increase boosting / reduce firing
- Case 3** – batch redox number correction (use of in-line redox sensor)

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Case 1 Redox control – Heat transfer

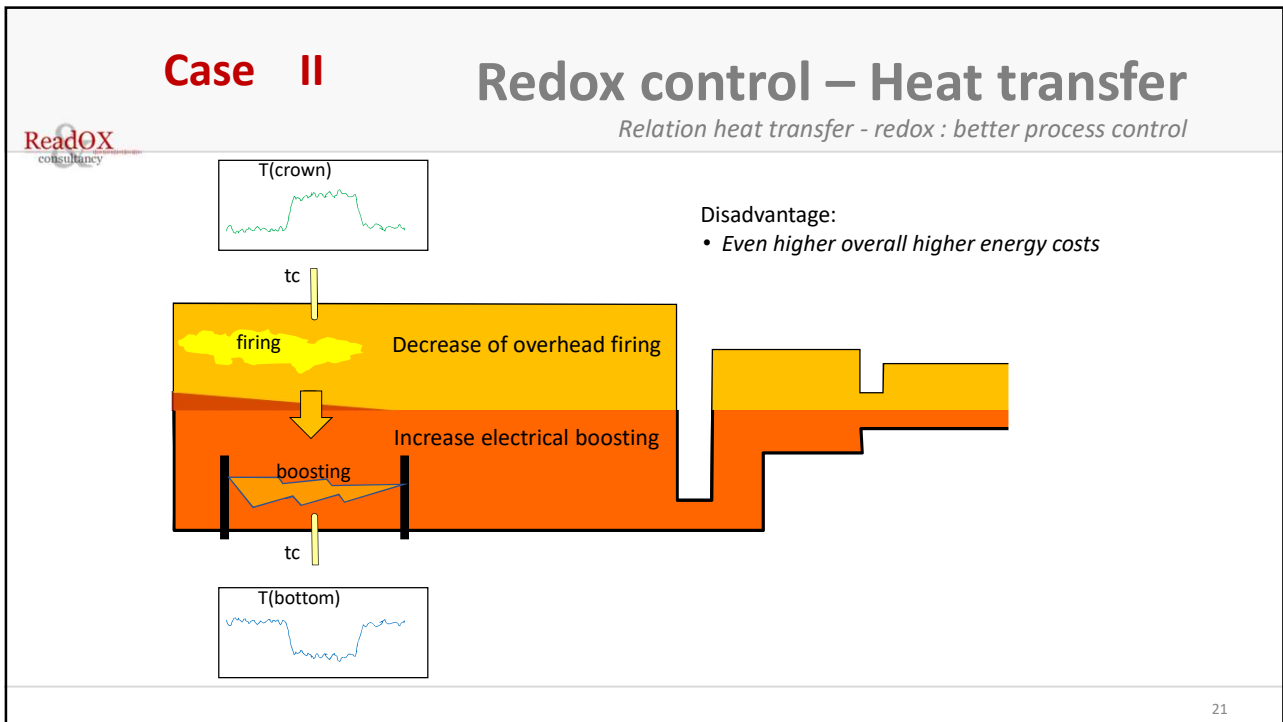
Relation heat transfer - redox : better process control

Disadvantages:

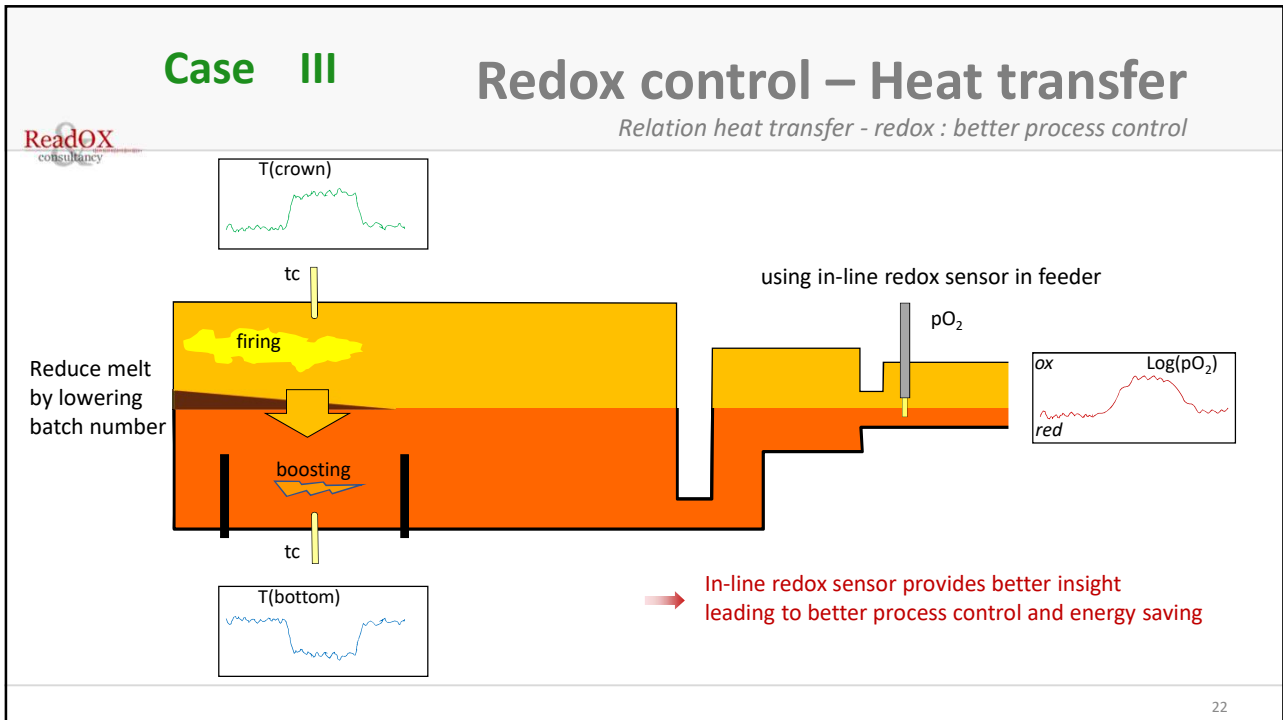
- Extra fuel costs
- Even higher crown temperature

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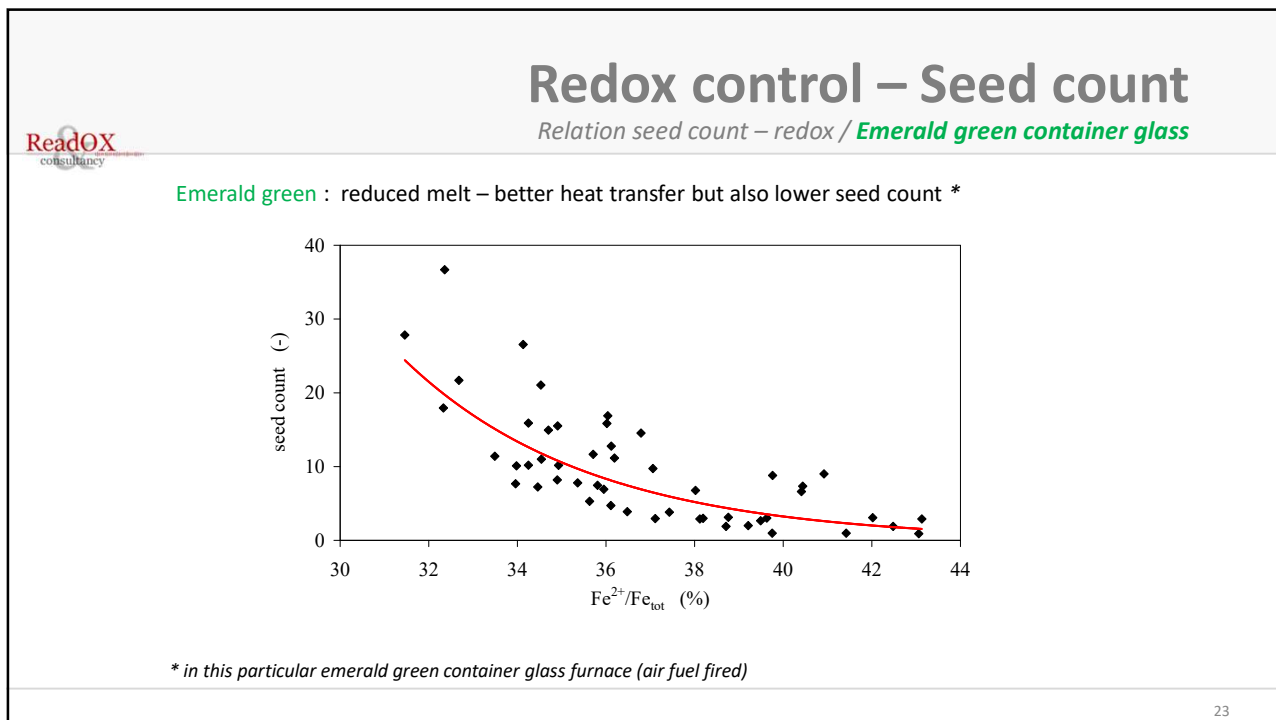
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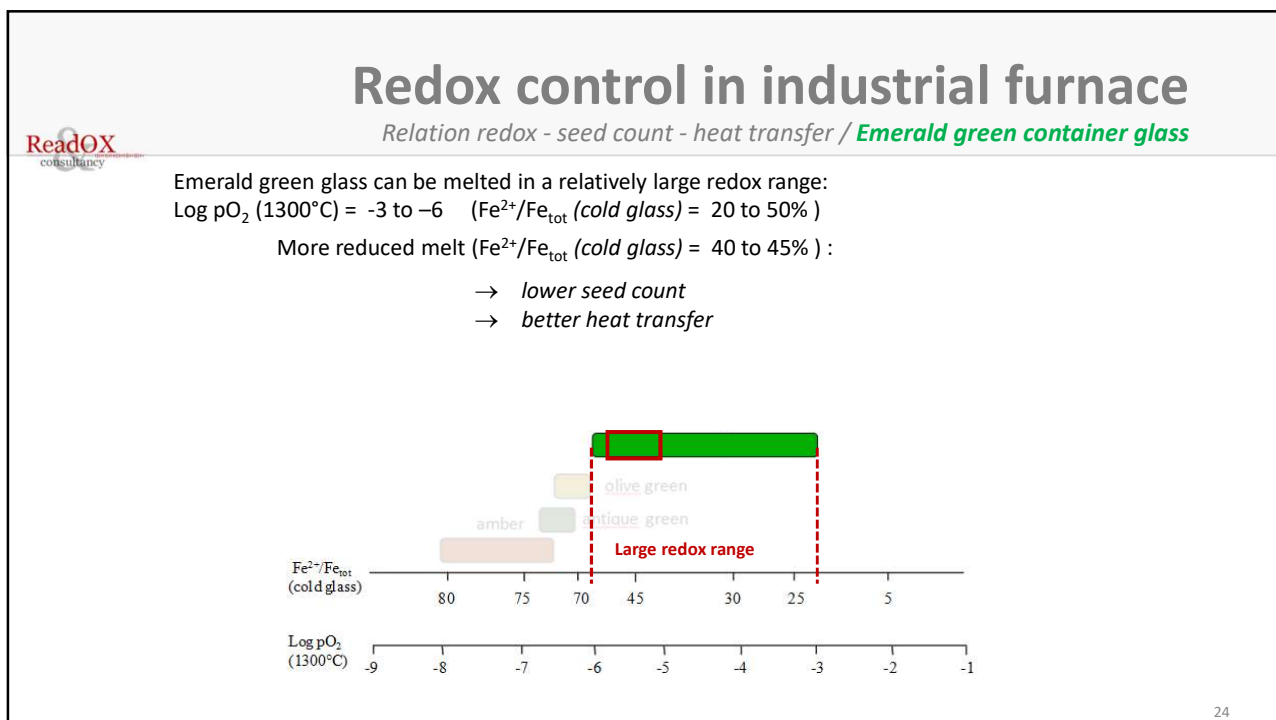
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Redox control in industrial furnace

Relation redox - seed count - heat transfer / Emerald green container glass

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Emerald green glass can be melted in a relatively large redox range:
 Log pO₂ (1300°C) = -3 to -6 (Fe²⁺/Fe_{tot} (cold glass) = 20 to 50%)

Risk of melting more reduced :
 melting foreign recycling cullet with incidentally high COD
 → amber cords and/or blisters may appear in the green glass

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Redox control in industrial furnace

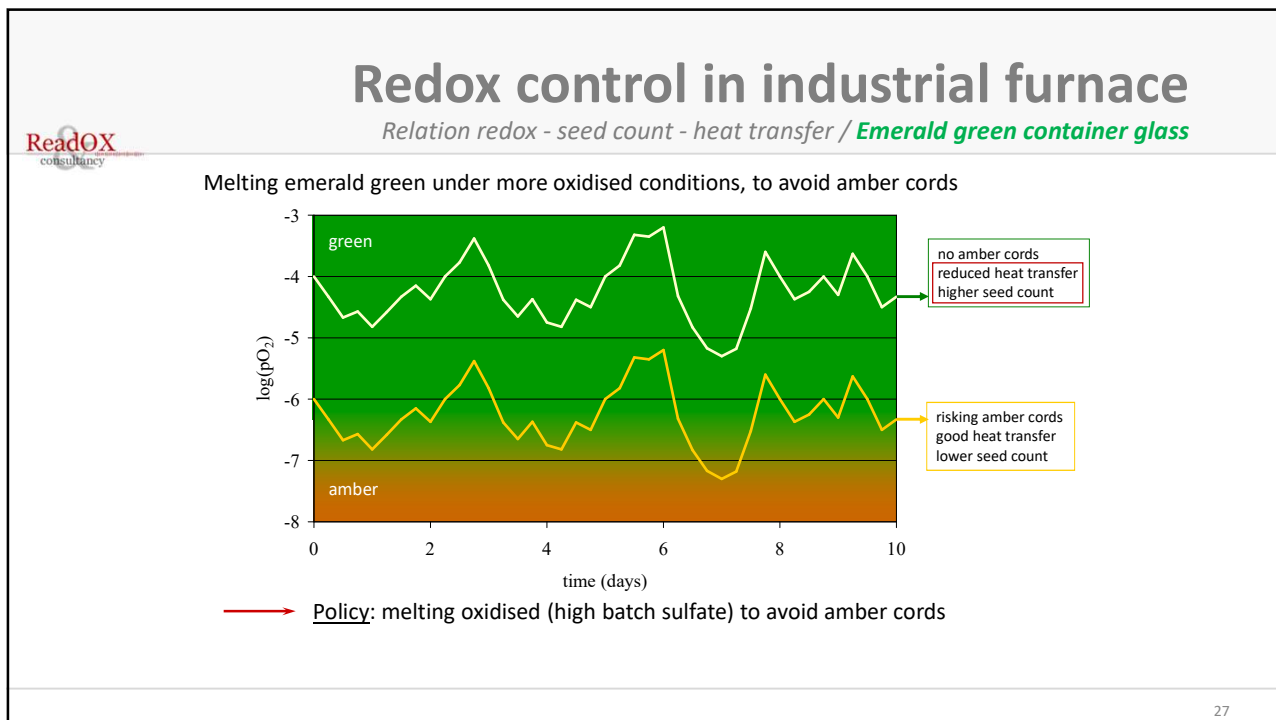
Relation redox - seed count - heat transfer / Emerald green container glass

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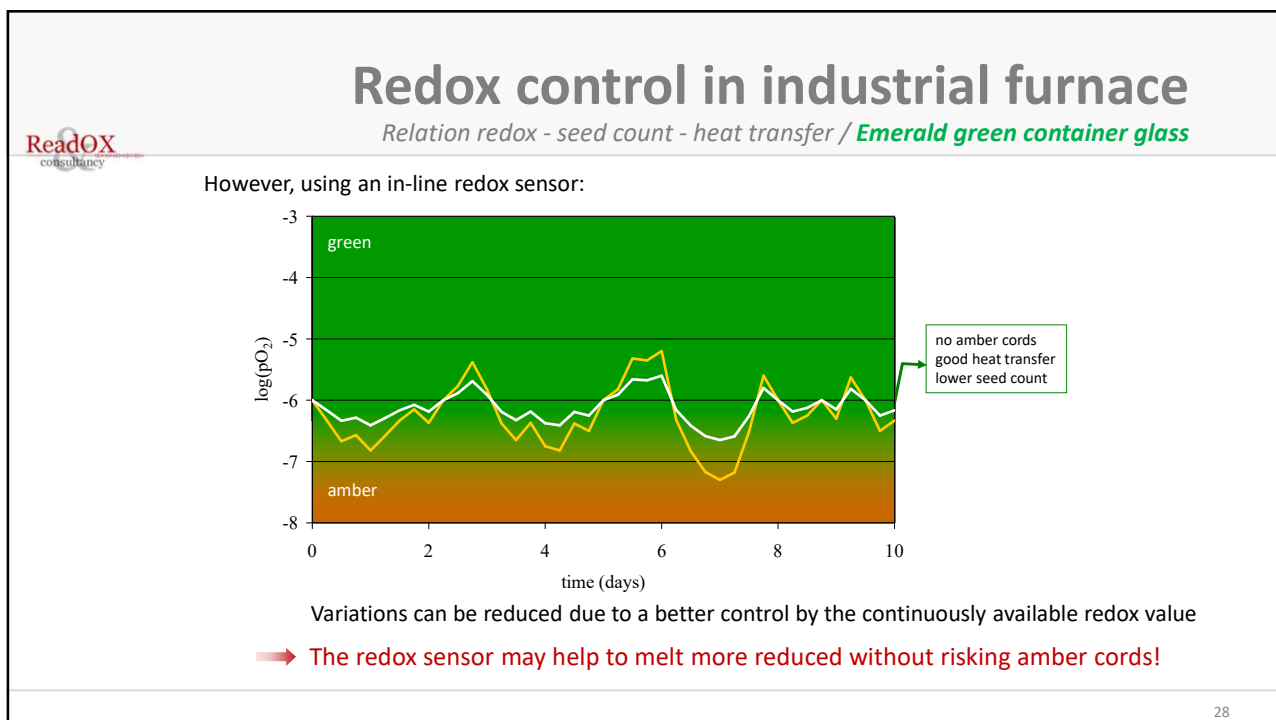
Melting emerald green under reduced conditions, with high levels of foreign recycling cullet:

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Redox control in industrial furnace

Colour control of green glasses with an amber colour component

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Antique green, olive green and dead leaf are very sensitive to redox variations

Mix of green and amber:

Cr³⁺

Fe²⁺/Fe³⁺

$$\begin{array}{c} \text{O}^{2-} \\ | \\ \text{O}^{2-}-\text{Fe}^{3+}-\text{S}^{2-} \\ | \\ \text{O}^{2-} \end{array}$$

Amber chromophore
Colour intensity ~ [Fe³⁺].[S²⁻]

Out of colour specification already as a result of small changes in :

- firing condition (air/fuel ratio)
- weathering degree of recycling cullet
- batch humidity
- pull

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Redox control in industrial furnace

Green glasses with an amber colour component : Olive green

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Fe₂O₃ and SO₃ (wt%)

log (pO₂(bar))

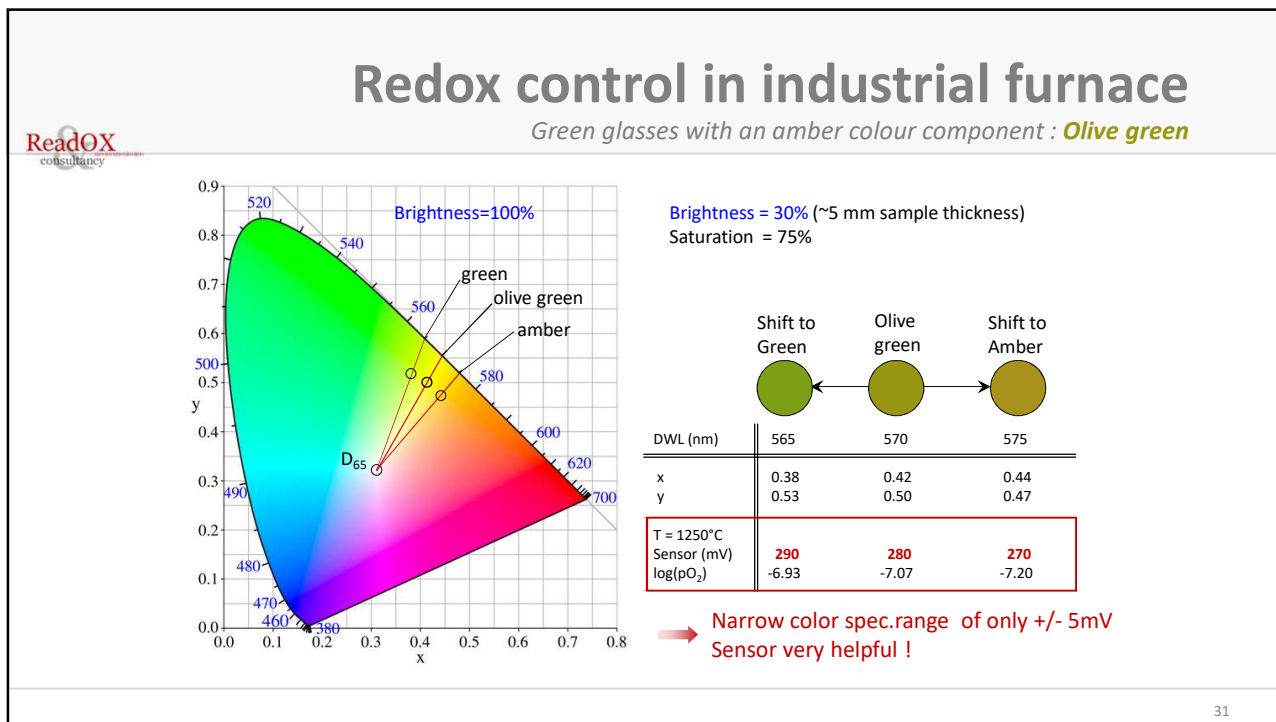
Amber chromophore
Colour intensity ~ [Fe³⁺].[S²⁻]

Olive green colour must be melted at the onset of the amber chromophore formation

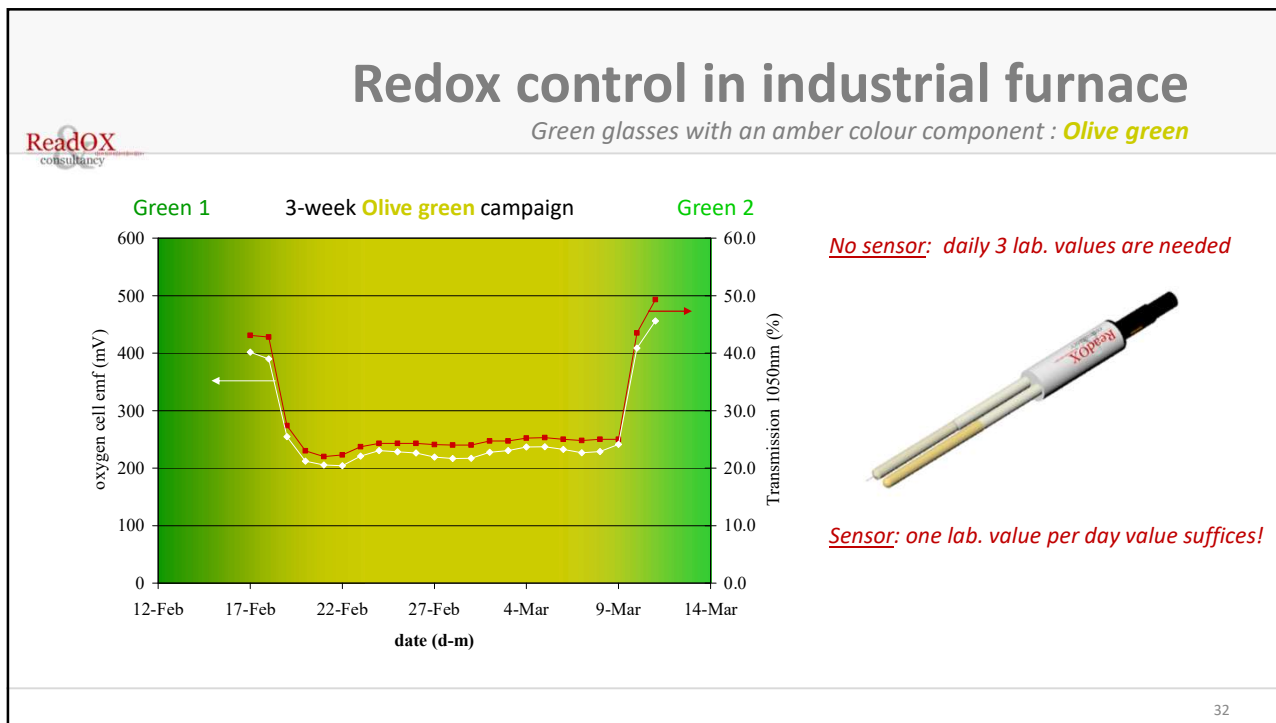
➔ **Narrow redox operating window**

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Redox control in industrial furnace

*Green glasses with an amber colour component : **Antique green***


Antique green is also very sensitive to redox variations (problem: over-reduction!)

Amber in flint:



Fe^{2+}/Fe_{tot} 0.50 0.80

Antique:
Amber in chromium green :



Fe^{2+}/Fe_{tot} 0.50 0.80

Data/Pictures by courtesy of Fehiman Akmaz, ŞİŞECAM

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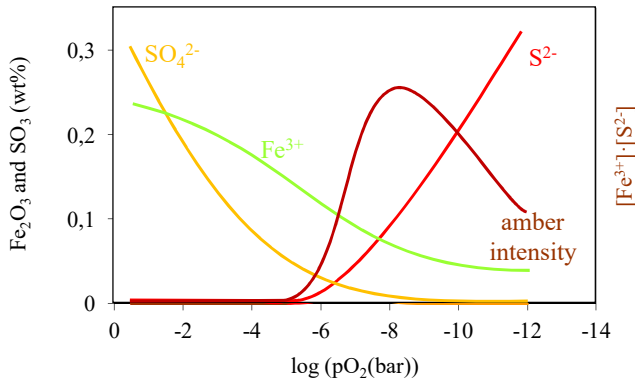
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Redox control in industrial furnace

*Green glasses with an amber colour component : **Antique green***

Antique green is sensitive to over-reduction

Amber in flint :

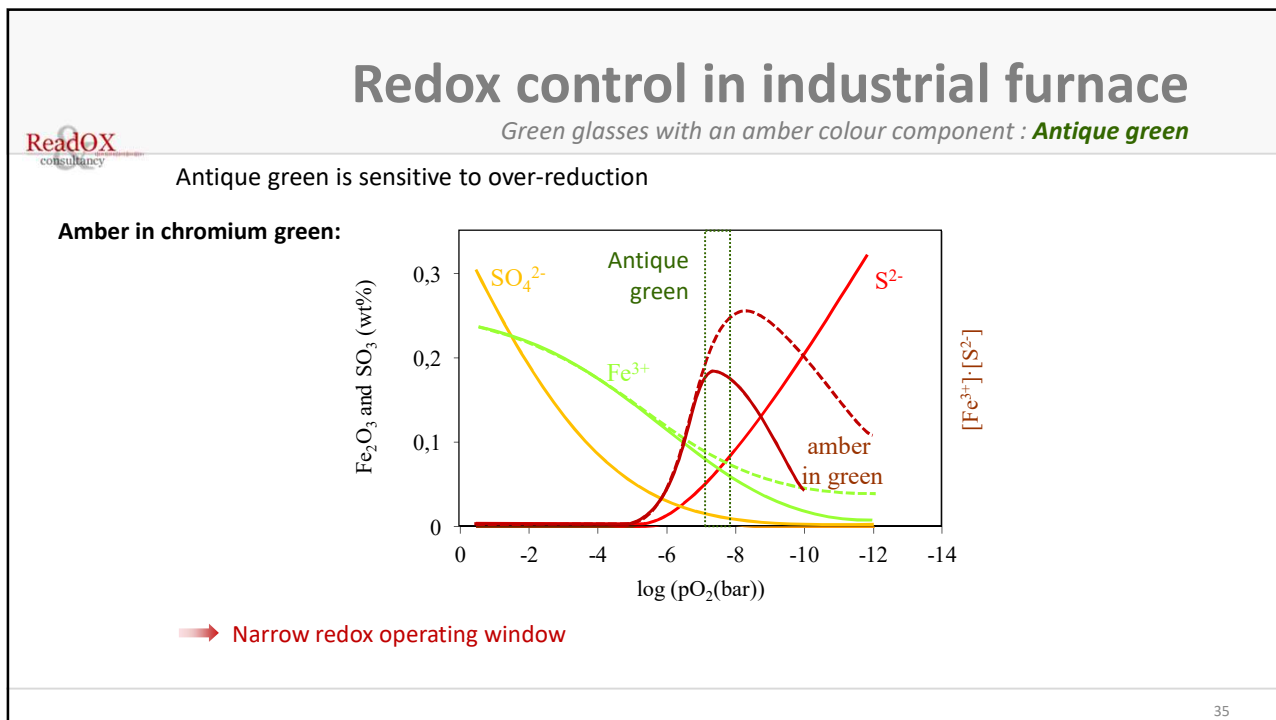


Fe_2O_3 and SO_3 (wt%) $[Fe^{3+}]$, $[S^{2-}]$

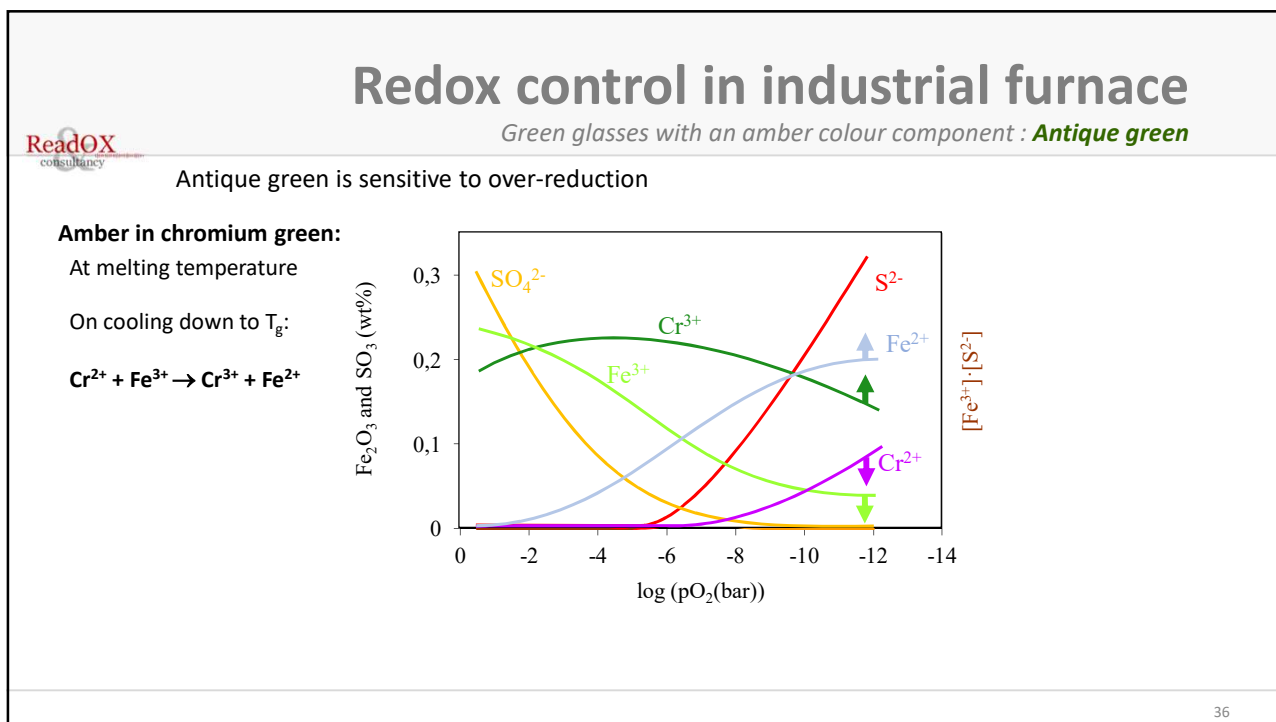
$log(pO_2)$ (bar)

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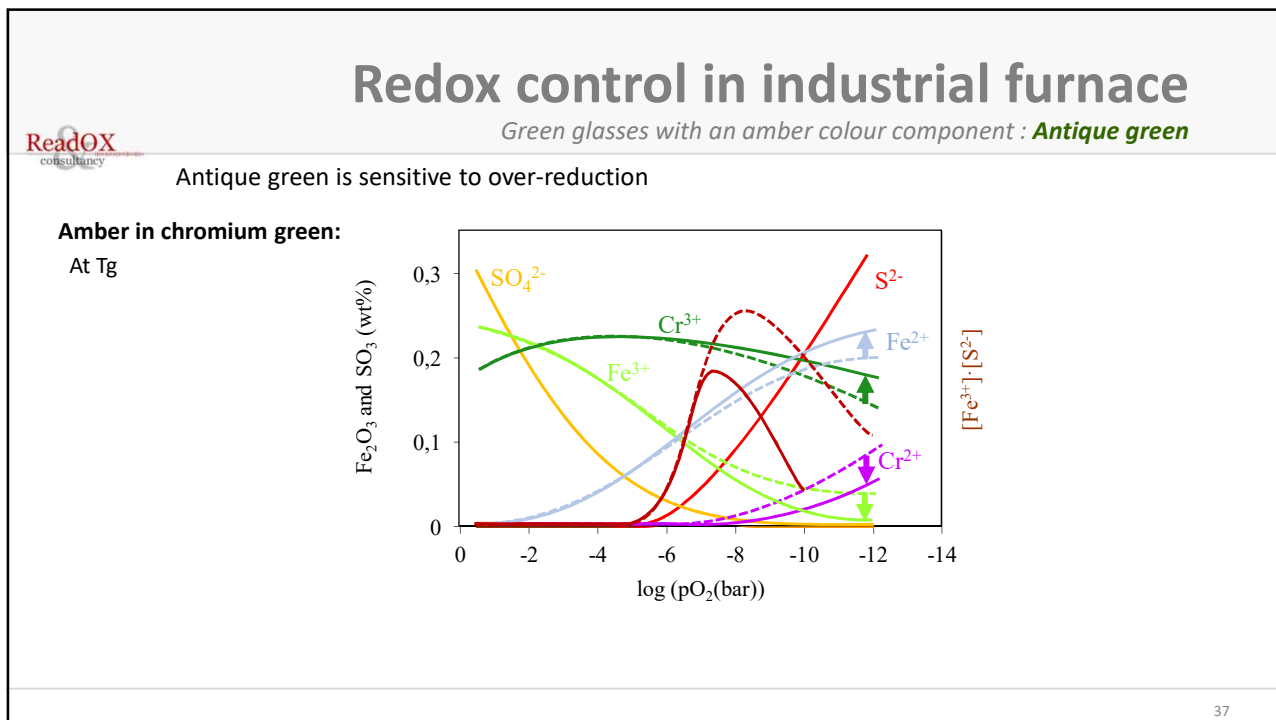
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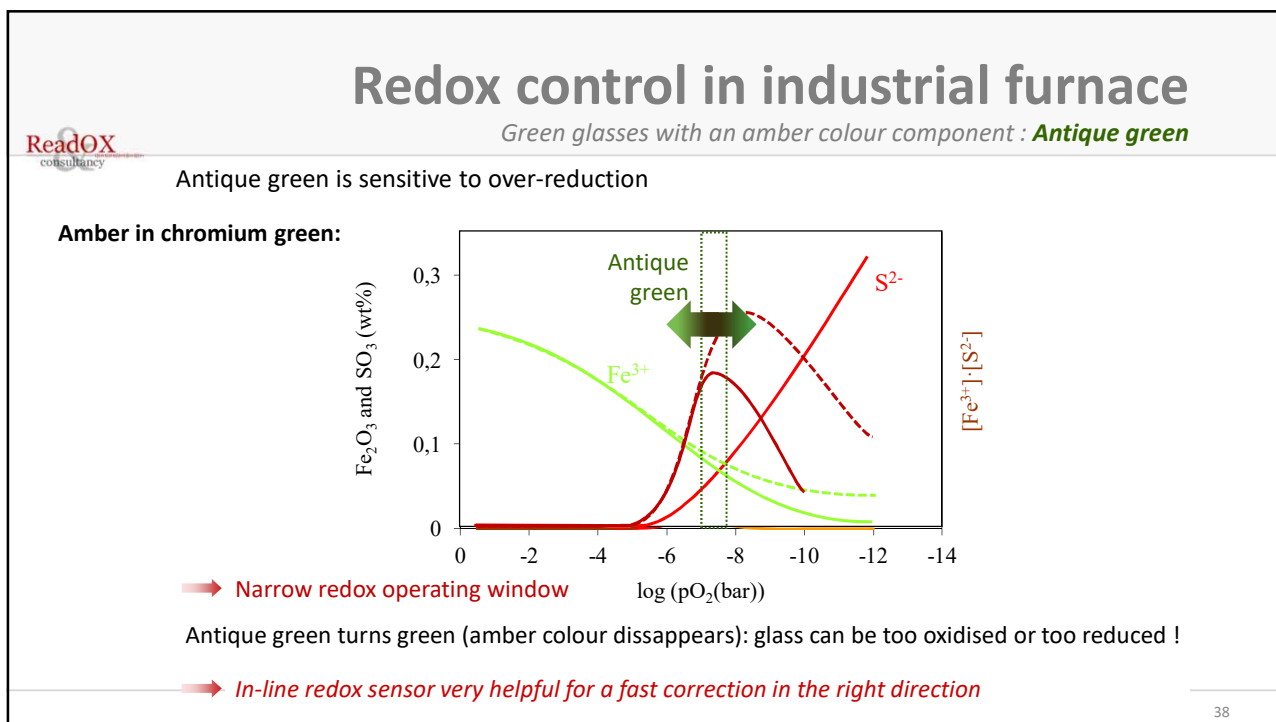
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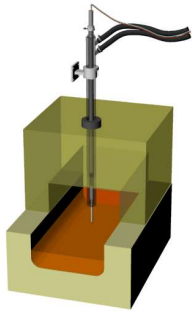
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Redox control : continuous iron ratio


Iron-ratio cold glass as continuous sensor output (with lab. calibration)

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Present situation: redox sensor gives $\log pO_2$ of the melt



$\log(pO_2)$?



Operator is used to work with daily lab analysis Fe^{2+}/Fe_{tot}





Semi-empirical relation

$Fe^{2+}/Fe_{tot}(\text{cold glass product}) = f(EMF, T)$

→

"lab-analysis" continuous available !!





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Redox control : continuous iron ratio

Iron-ratio cold glass as continuous sensor output (with lab. calibration)

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Continuous iron-ratio is the sum of an iron-ratio calibration value (laboratory) and an (empirical) function of the EMF change and T change:

$$(Fe^{2+}/Fe_{tot})_t = \underbrace{(Fe^{2+}/Fe_{tot})_0}_{\text{laboratory}} + \underbrace{f(\Delta EMF, \Delta T)}_{\text{sensor}}$$

$(Fe^{2+}/Fe_{tot})_t$ = continuous iron-ratio of cold glass (sensor output)



$(Fe^{2+}/Fe_{tot})_0$ = iron-ratio calibration value (laboratory spectrometer)

ΔEMF = $EMF_t - EMF_0$

ΔT = $T_t - T_0$

At calibration procedure estimation of $t=0$

Glass melt → Bottle → Lab result

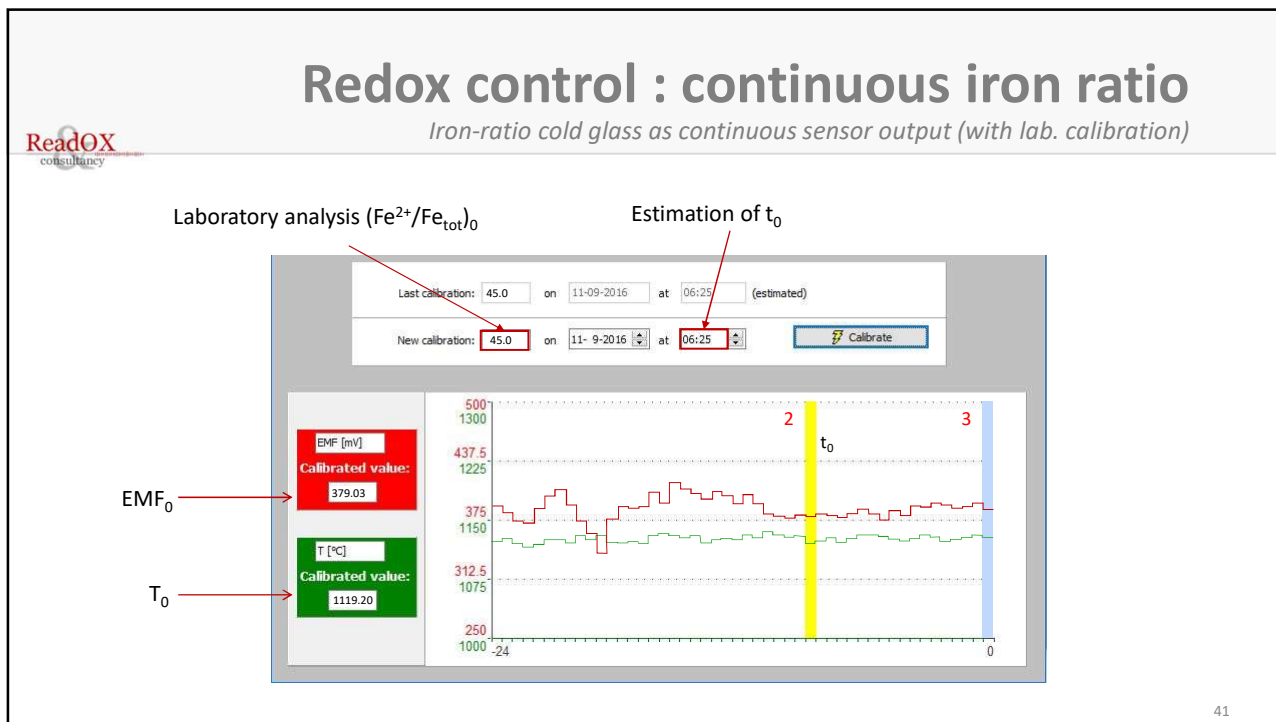
$(\frac{Fe^{2+}}{Fe_{tot}})_0$

t=0 : time at which the (later) analysed cold glass sample passed the sensor (EMF_0 and T_0) as a glass melt

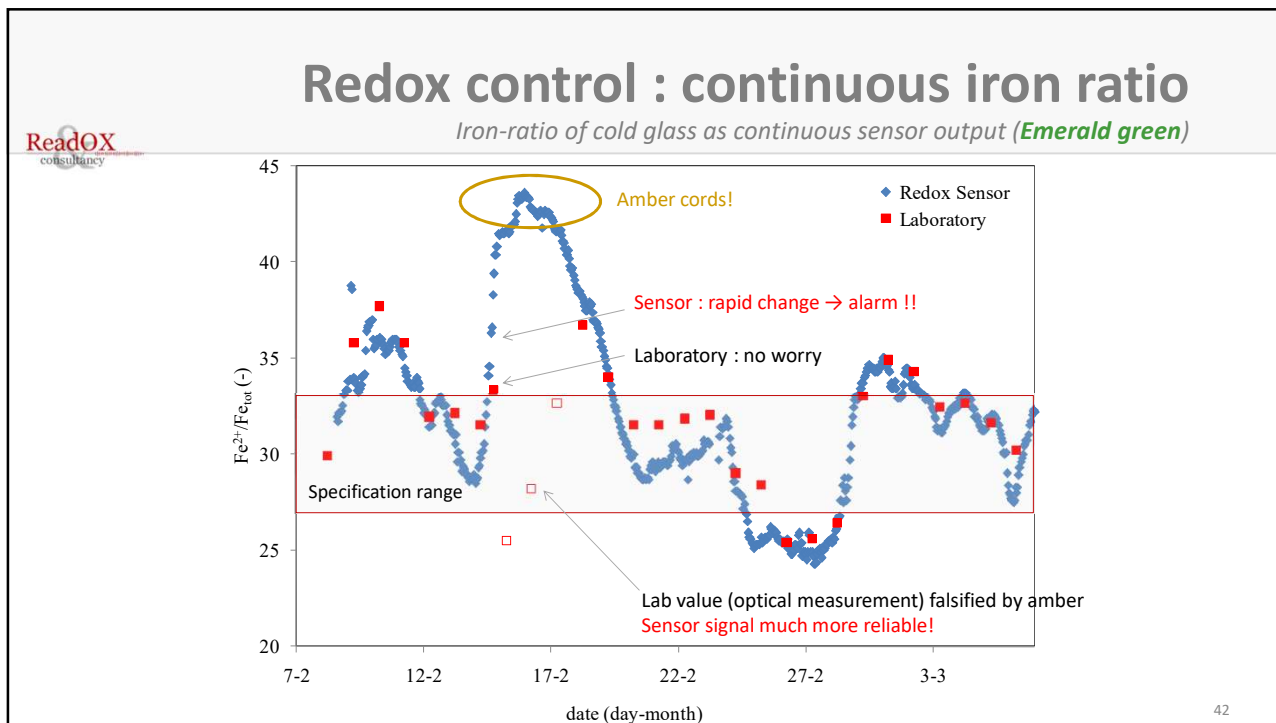
$t=0 : EMF_0$ and T_0

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Redox control : continuous iron ratio

Iron-ratio cold glass as continuous sensor output (with lab. calibration)



Continuous iron ratio of cold glass - Advantages:

- No miscommunication between lab and furnace operators
- Lab: single iron-ratio value once a day
Sensor: continuous (level, direction and rate of change)

➔ In a few emerald green furnaces the continuous iron-ratio is running with great satisfaction

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Concluding remarks

Advantages of using an in-line glass melt redox measuring system



Continuous use:

- Always redox state available for monitoring and for fast correction
 - *Container glass with high levels of recycling cullet (energy saving by optimal heat transfer, colour stability and low seed count)*
 - *Glasses with narrow colour specifications (olive green, dead leaf, antique green)*

Occasional use:

- During a colour conversion (faster conversion without overshoot)
- During a campaign of a redox sensitive colour
- Batch recipe changes (new material supplier)
- Trouble shooting (is redox causing the process instability or product defect?)
- Research program: relation process/product parameters to glass melt redox (Big Data: PCA)

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New developments

Advantages of an in-line glass melt redox measuring system



New developments:

- For float glass lines: Nickel free stainless steel redox measuring system (water-cooled jacket, measuring lance)
- Glass melt redox sensor with high internal resistance (higher EMF stability in (ultra) clear glasses, with low levels of multivalent ions)

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SPECIAL MEASURING REQUIREMENTS ?

in glass melt, molten metal and salts

Contact us !

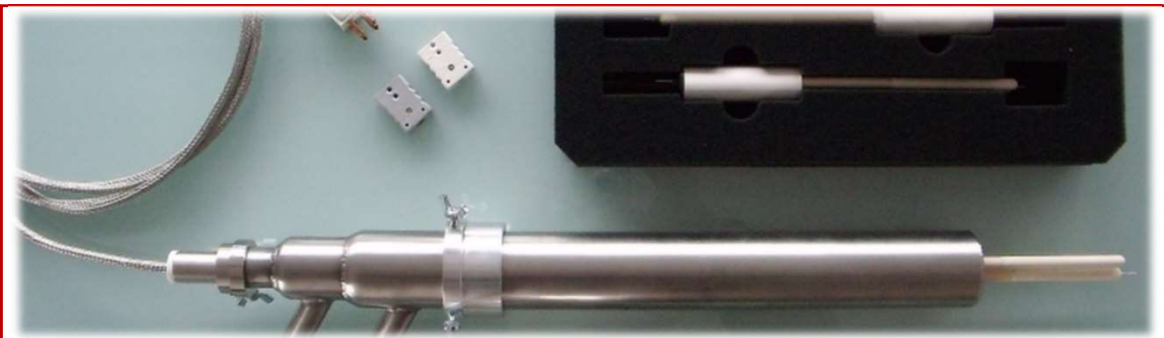
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